

NON-PUBLIC?: N
ACCESSION #: 9306170076
LICENSEE EVENT REPORT (LER)

FACILITY NAME: Monticello Nuclear Generating Plant PAGE: 1 OF 6

DOCKET NUMBER: 05000263

TITLE: Reactor Protection System Actuation From High Pressure
Caused By Inadequate Procedure
EVENT DATE: 03/23/93 LER #: 93-006-01 REPORT DATE: 06/09/93

OTHER FACILITIES INVOLVED: DOCKET NO: 05000

OPERATING MODE: N POWER LEVEL: 10%

THIS REPORT IS SUBMITTED PURSUANT TO THE REQUIREMENTS OF 10 CFR
SECTION:
50.73(a)(2)(iv)

LICENSEE CONTACT FOR THIS LER:
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I&C Engineering

COMPONENT FAILURE DESCRIPTION:
CAUSE: B SYSTEM: AA COMPONENT: SOL MANUFACTURER: A609
REPORTABLE NPRDS: Y

SUPPLEMENTAL REPORT EXPECTED: NO

ABSTRACT:

During startup from a refueling outage a Reactor Protection System trip from high reactor pressure occurred. The trip occurred while performing the main turbine Stop Valve tightness test. The cause of the event was an inadequate procedure. Contributing factors were inadequate knowledge by the individuals involved in the procedure revision, incorrect simulator modeling and an inadequate vendor technical manual procedure. During the event one control rod scram solenoid failed to operate resulting in a slow rod insertion time. The Turbine Stop and Control Valve Tightness Test procedure has been revised. The plant simulator was modeled to reflect actual operation. The failed scram solenoid pilot valve was replaced and all scram solenoid pilot valves were verified to function properly. This event and the lessons learned from the event will be presented in Engineering Technical Staff Continuing Training and License Operator Requalification training. The vendor technical manual

on pressure control will be revised.

END OF ABSTRACT

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Description

On March 23, 1993, at 0618 hours, during startup from a refueling outage, a Reactor Protection System (EIS System: JC) trip from high reactor pressure occurred. With the reactor at about 10% rated power and 940 psig, a surveillance procedure, Main Turbine Stop and Control Valve Tightness Test, was being performed. The Steam Pressure Control System (EIS System: JI) was controlling reactor pressure using the Main Steam Bypass Valves (EIS Component: V). The Mechanical Pressure Regulator was controlling with the Load Limit set at 100%. The Main Turbine (EIS Component: TRB) was at 1800 RPM under control of the Speed Load Changer. In the performance of the procedure the stop valves are closed and it is verified that the turbine decelerates to 1200 RPM. When the Stop Valves were closed the turbine began to decelerate and reactor pressure began to increase slowly. After about 110 seconds the Bypass Valves began to close and reactor pressure began increasing more rapidly. A full scram on high reactor pressure occurred 137 seconds after the Stop Valves were closed. One safety relief valve (EIS Component: RV) operated in the Low-Low Set mode. Immediately following the scram the operator noticed that all control rods (EIS System: AA) were not full in as indicated by the one-rod-out permissive light. The Rod Worth Minimizer Display indicated one control rod not full in. Shortly there-after all control rods indicated full in by all indications. Subsequent review of control rod scram times recorded by the Rod Worth Minimizer revealed that one control rod exhibited a delayed scram. All other systems functioned as designed. The immediate and subsequent procedure actions for the scram were performed.

This event resulted in an automatic trip of the Reactor Protection System and is reportable per 10CFR50.73(a)(2)(iv).

Cause

Investigation of the event determined that the Steam Pressure Control system performed as designed.

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To understand the following explanation, refer to the attached Figure 1, Main Steam Pressure Control Functional Control Diagram. Stop Valve

closure terminated steam flow to the turbine. This initiated a slow increase in reactor pressure and allowed the turbine to decelerate. The increase in reactor pressure resulted in a slowly increasing output from the Mechanical Pressure Regulator. The decrease in turbine speed resulted in an increasing output from the Speed Governor. Initially, the output of low value gate 3 (LVG3 on Figure 1) was limited by the speed governor signal. The difference between the pressure signal and the output of LVG3, minus a bias of 3%, (output of E4) controlled the opening of the bypass valves. Since the output of LVG3 was increasing at about the same rate as the pressure signal, the bypass valves did not respond to the initial slow pressure increase. When the pressure signal reached the setting of the Flow Limit, the pressure signal applied to E4 was held at the limited value (105%). As the speed signal to LVG3 continued to increase, the difference signal (output of E4) decreased, and the bypass valves began to close. This caused a faster pressure increase.

The cause of the event was an inadequate procedure. The procedure was revised on March 3, 1993. During the revision process a step to place the Load Limit to 25% to limit the speed governor signal was deleted. The revised procedure was validated on the plant simulator, but subsequent investigation has determined that the simulator did not model the control system correctly. Contributing factors identified were inadequate knowledge by the Licensed Operators and system engineer involved in the procedure revision, incorrect simulator modeling and an inadequate procedure in the vendor technical manual for the steam pressure control system. The vendor manual provided direction to fully open the control valves but did not provide a caution concerning the operation of the flow limiter.

The single control rod delayed scram was determined to be caused by a scram solenoid pilot valve (EHS Component: SOL) which did not function. The solenoid was one of 154 replaced during the 1993 refueling outage. Post maintenance testing had verified proper operation prior to start-up. The valve was disassembled and inspected. Separation of the solenoid core from the core spring had occurred due to improper assembly by the manufacturer. Separation cannot occur with proper assembly. Bench testing confirmed that, after improper assembly, failure would occur after several valve cycles.

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Analysis

This event represents an unnecessary challenge to the Reactor Protection System and an unnecessary plant transient. All systems responded as

designed and all parameters remained within analyzed values with the exception of the delayed control rod scram. Since the Stop Valve Tightness test is only performed at low power levels this event could not have occurred under other conditions which would have resulted in more severe consequences. There were no consequences to the health and safety of the public.

The failure of the scram solenoid pilot valve was determined to be an isolated case. All 22 spare solenoid valves were inspected and were found to be properly assembled. Each installed solenoid was cycled five times and verified to function properly.

A single rod delayed scram which occurs due to the action of the backup scram valves represents an insignificant decrease in scram reactivity insertion rate. The Technical Specifications contain Limiting Condition for Operations (LCOs) governing core average and four rod array scram times. These LCOs were not exceeded.

Corrective Actions

The following actions have been completed:

1. The Turbine Stop and Control Valve Tightness Test procedure has been revised.
2. The plant simulator was revised to properly model operation of the Steam Pressure Control System.
3. The failed scram pilot solenoid valve was replaced and all installed scram pilot solenoid valves were cycled and verified to function properly.
4. All remaining solenoids of this type in stock were inspected and no other problems were found.

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The following actions will be completed:

1. This event and the lessons learned from the event will be presented in Engineering Technical Staff Continuing Training. This training will emphasize the importance of procedure development and technical review.
2. This event will be presented in Licensed Operator Requalification Training. The training will include use of the simulator to

demonstrate the proper operation of the Steam Pressure Control System.

3. The simulator software change process will be revised to include independent review by a qualified individual.

4. A revision to the vendor technical manual will be issued providing guidance on performing the stop valve leak tightness test.

Additional Information

Failed Component Identification

Scram Pilot Solenoid Valve

Manufacturer: ASCO

Model: HVA 90-405

Previous similar events

None

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Figure 1 "Main Steam Pressure Control Functional Control Diagram" omitted.

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NSP Northern States Power Company

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Minneapolis, Minnesota 55401-1927

Telephone (612) 330-5500

June 9, 1993

Report Required by

10 CFR Part 50, Section 50.73

US Nuclear Regulatory Commission

Attn: Document Control Desk

Washington, DC 20555

MONTICELLO NUCLEAR GENERATING PLANT

Docket No. 50-263 License No. DPR-22

Reactor Protection System Actuation

From High Pressure Caused By Inadequate Procedure

The supplemental Licensee Event Report for this occurrence is attached.
This report contains the following new NRC commitment.

A revision to the vendor technical manual will be issued
providing guidance on performing the stop valve leak
tightness test.

Please contact Marv Engen, Sr Licensing Engineer, at (612) 295-1291 if
you require further information.

Roger O Anderson
Director
Licensing and Management Issues

c: Regional Administrator - III, NRC
NRR Project Manager, NRC
Sr Resident Inspector, NRC
State of Minnesota
Attn: Kris Sanda

Attachment

*** END OF DOCUMENT ***
